Introduction to Data Reduction

EuroWinter School

Observing with the Very Large Telescope Interferometer

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Topics

System Analysis Data processing

- •The perturbed wavefront •Diffraction effects: the pupil function •Image spectrum: the transfer function •The field of view
- •Spatial filtering

- The observables
- Interferometric equation
- •Temporal coding
- •Wavelet analysis
- Spatial coding
	- Visibility
	- –Differential phase
	- Closure phase
- The AMBER case

The perturbed wavefront

- $\Psi_o(x)$ Object wavefront \rightarrow •
- $e^{i\phi(x,t)}$ Atmospheric effects \rightarrow \bullet
- $\Psi(x,t) = \Psi_o(x) e^{i\phi(x,t)}$ Perturbed wavefront \rightarrow \bullet

The perturbed wavefront is defined by $N_s = \left(\frac{D_r}{r_0^2}\right)^2$ and N_s

Calibration problems

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Diffraction effects: the pupil function

- $A(\alpha, t) \propto \int_{Aperture} \Psi(x, t) e^{-2i\pi \alpha \frac{x}{\lambda}} dx$ • Fraunhofer diffraction \rightarrow
- Pupil function with $\rightharpoonup P(u)$ with

 $A(\alpha, t) \propto \int \Psi(u, t) P(u) e^{-2i\pi \alpha u} du$

 $A(\alpha, t) \propto FT[\Psi(u,t)P(u)]$

The diffracted field is proportional to the Fourier transform of the input field

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Image spectrum: the ideal transfer function

 $I(\alpha) = \langle |A(\alpha)|^2 \rangle \propto \langle |FT[\Psi_o(u)P(u)]|^2 \rangle$ Image plane intensity distribution \rightarrow $I(f) \propto \int \langle \Psi_{o}^{*}(u) \Psi_{o}(u+f) \rangle P^{*}(u) P(u+f) du$ Image spatial spectrum \rightarrow $\langle \Psi_{o}^{*}(u)\Psi_{o}(u+f)\rangle \propto O(f)$ Zernike-van Cittert theorem \rightarrow $I(f) = O(f).T(f)$ Image spectrum \rightarrow $T(f) = \frac{1}{s} \int P(u)P^*(u+f)du$ Ideal transfer function \rightarrow

The field of view (FOV)

- Theorem: the Fourier transform of a periodic function with period is L • $\Delta f = \frac{1}{L}$ *discrete* at points separated with
- •These points are called *independant points*
- If we know the Fourier components of an image with a sampling interval •, it is then p is b^1 to reconstruct a field \boldsymbol{L}
- • Single telescopes have continous transfer function \rightarrow the FOV is only limited by geometrical constraints
- • Diluted telescopes have discontinous transfer function \rightarrow the FOV is limited by the sampling of the pupil plane

Importance of positivity and *support* for image reconstruction

Spatial filtering

- \bullet Non fibered (multimode) interferometers transmit the object spectrum over the support of the transfer function
- \bullet Optical fibers \rightarrow $A(\alpha, t) = c(t)G(\alpha)$
- •Transform $N_s = \left(\frac{D}{r_0}\right)^2$ random phases into 1 random flux
- • Fibered (monomode) interferometers transmit the mean object spectrum over the pupil

the FOV is limited to one Airy disc

Data processing: the observables

•Object spatial spectrum \rightarrow $O(f) = \frac{\int O(\alpha)e^{-2i\pi f\alpha}d\alpha}{\int O(\alpha)d\alpha}$

- • The observables
	- The visibility \rightarrow
	- The differential visibility \rightarrow
	- The differential phase \rightarrow
		- The closure phase \rightarrow

 $V(f)$ $V(f,\sigma_1)/V(f,\sigma_2)$ $\phi_d = \phi(\sigma_1) - \phi(\sigma_2)$ $\phi_c = \phi_{12} + \phi_{23} - \phi_{13}$

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Data processing: starting point

- • Data processing starting point, data corrected from
	- –Detector bias
	- Flat field
	- –Bad pixels
- • The 3 basic signals per frame:
	- –1 interferometric signal \rightarrow
- $S'(z) = S(z) + B(z)$

2 photometric signals

$$
P_1^{\prime}(z)=K_1(z)+B_1(z)
$$

$$
P_2^{\prime}(z)=K_2(z)+B_2(z)
$$

Interferometric equation

- $|\Psi_1(\sigma)+\Psi_2(\sigma)|^2*g(\sigma)$ Beam recombinaison \rightarrow •
- •Interferometric equation: $z = t$ (MIDI) or $z = \alpha$ (AMBER)

 $S'(z) = K_1(z) + K_2(z) + 2Vq(z + \Delta z, \delta \sigma) \sqrt{K_1(z)K_2(z)} cos \Phi(z) + B(z)$ $\Phi(z) = 2\pi f_c(z + \Delta z) + \phi_s + \phi_a$

•Temporal coherence effect (assuming square spectral filter)

$$
q(z+\Delta z, \delta \sigma) = sinc \big[f_c(z+\Delta z) \frac{\delta \sigma}{\sigma} \big]
$$

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Pre-processing: 1st order bias corrections

 \bullet Photometric bias corrections

$$
S(z) = S'(z) - \langle B(z) \rangle
$$

\n
$$
P_1(z) = P'_1(z) - \langle B_1(z) \rangle
$$

\n
$$
P_2(z) = P'_2(z) - \langle B_2(z) \rangle
$$

•The MIDI case

Temporal coding (MIDI)

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Temporal coding: the visibility (1)

 \bullet Interferometric equation

 $S(t) = K_1(t) + K_2(t) + 2 V \sqrt{K_1(t)K_2(t)} sinc\big[(vt+d)\delta\sigma\big]cos\Phi(t)$

 $\Phi(t) = 2\pi vt\sigma + 2\pi d\sigma + \phi_s + \phi_o$

 \bullet Correction of the interferogram

$$
s(t) = \frac{S(t) - P_1(t) - P_2(t)}{\sqrt{P_1(t)P_2(t)}} = 2V\operatorname{sinc}\left[(vt + d)\delta\sigma\right]\cos\Phi(t)
$$

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Temporal coding: an example of interferogram Temporal coding: an example of interferogram

Temporal coding: the visibility extraction Temporal coding: the visibility extraction

 $s(\nu) = s^+(\nu) + s^-(\nu)$ Spectrum \rightarrow •

$$
<\ \Big|\ s^+(\nu) d\nu> = V e^{i\phi_0} e^{i\phi_s}
$$

Not a good estimator of the visibility

•Power spectrum \rightarrow $\langle \int |s^+(\nu)|^2 d\nu \rangle = V^2 + \langle b \rangle$

Good estimator of the visibility \rightarrow to be corrected for system visibility (calibrator)

- •Avantage of temporal coding \rightarrow insensitive to the OPD
- •Inconvenient \rightarrow sensitive to opd distorsions (relaxed at 10 μ m for MIDI)

Þ

Temporal coding: wavelet analysis Temporal coding: wavelet analysis

- Wavelet analysis could be a powerful tool to analyse temporal interferograms
- Allow to make a analysis of possible OPD variations along the interferogram
- \rightarrow tool to test the quality
- Better estimate of the visibility?
- \rightarrow to be investigated further

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Spatial coding (standard)

Spatial coding: the visibility (1)

•Interferometric equation

 $S(\alpha) = K_1 a_1(\alpha) + K_2 a_2(\alpha) + 2V \sqrt{K_1 K_2} \sqrt{a_1(\alpha) a_2(\alpha)} sinc [(b\alpha + d)\delta\sigma] cos\Phi(\alpha)$

$$
\Phi(\alpha) = 2\pi b \alpha \sigma + 2\pi d \sigma + \phi_s + \phi_o
$$

•Continuum correction

 $s(\alpha) = S(\alpha) - P_1(\alpha) - P_2(\alpha) = 2V\sqrt{K_1K_2}\sqrt{a_1(\alpha)a_2(\alpha)}sinc[(b\alpha+d)\delta\sigma]cos\Phi(\alpha)$

Spatial coding: the visibility (standard 1)

• Spectrum \rightarrow

 $<\int s^+(f)df>=Ve^{i\phi_o}e^{i\phi_s}\sqrt{a_1(0)a_2(0)}<\sqrt{K_1K_2}sinc(d\delta\sigma)e^{2i\pi d\sigma}>0$

Not a good estimator of the visibility

•Power spectrum

 $<\int |s^+(f)|^2 df> = V^2 \int a_1(\alpha)a_2(\alpha) < K_1K_2sinc^2[(b\alpha+d)\delta\sigma] > d\alpha$

Sensitive to the OPD

Spatial coding: the visibility (standard 2)

- \bullet Necessity to correct each interferogram for the non zero OPD
- •Phase of the interferogram $2\pi d\sigma + \phi_s + \phi_s$ function of the OPD
- • d estimated from the slope of the fringes
	- differential phase of
	- includes also dispersion within fibers (assuming linearity with σ)
- •Correction for the OPD

$$
m(\alpha) = \frac{s(\alpha)}{sinc[(b\alpha + d)\delta\sigma]} = 2V\sqrt{K_1K_2}\sqrt{a_1(\alpha)a_2(\alpha)}cos\Phi(\alpha)
$$

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Spatial coding: the visibility (standard 3)

 \bullet Power spectrum

$$
< \int |m^+(f)|^2 df> = V^2 < K_1 K_2 > \int a_1(\alpha) a_2(\alpha) d\alpha +
$$

 \bullet Scalar product of the photometric channels

$$
<\int P_1(\alpha)P_2(\alpha)d\alpha>=\int a_1(\alpha)a_2(\alpha)d\alpha
$$

- $V^2 = \frac{<\int |m^+(f)|^2 df > **0** } {<\int P_1(\alpha) P_2(\alpha) d\alpha >}$ The visibility •
	- correction of OPD jitter during integration easy

To be corrected for system visibility on calibrator

Spatial coding: the differential phase

 \bullet Cross spectrum at 2 different wavelengths

$$
\int s^+(f,\sigma_1)df\int s^{+*}(f,\sigma_2)df=Ge^{2i\pi d(\sigma_1-\sigma_2)+i(\phi_1-\phi_2)+\phi_s}
$$

- \bullet Non zero OPD estimated from the sope of the fringes as a function of σ
- \bullet Differential phase

$$
\phi_1-\phi_2=Arg\Bigl\langle e^{-2i\pi d(\sigma_1-\sigma_2)}\int s^+(f,\sigma_1)df\int s^{+*}(f,\sigma_2)df\Bigr\rangle-\phi_s
$$

- •Correction of dispersion within fibers (2nd order)
- \bullet System phase $\phi_{\text{salibrated}}$ with the beam commuter device (bcd) and calibrator \rightarrow problem of calibrators

Spatial coding: the closure phase (standard)

- •With N telescopes the standard method for visibility and phase extraction is based on the separability of the $Nx(N-1)/2$ high frequency peaks
- •The 3 telescopes case: 3 high frequency peaks in the spectrum

$$
s^+(f-f_{12}) \quad s^+(f-f_{23}) \quad s^+(f-f_{13})
$$

•Closure phase = bispectrum phase

 $\phi_{12} + \phi_{23} - \phi_{13} = Arg \left\langle \int s^+(f-f_{12}) df \int s^+(f-f_{23}) df \int s^{+*}(f-f_{13} df) \right\rangle - \phi_s$

•The system phase ϕ (gideally zero) is to be calibrated on a reference source

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The AMBER case

- • The 2 telescopes case
	- the 2 high frequency peaks are separated
	- previous formalism applicable
- • The 3 telescopes case
	- partial overlapping of the 3 frequency peaks to reduce the nb of pixels
	- previous formalism non applicable
	- need to work in the image plane by modelling each interferogram

The AMBER case: modelling the interferograms

•Continuum correction

 $m_k = S_k - P_{1k} - P_{2k} = 2V\sqrt{K_1K_2\sqrt{a_{1k}a_{2k}}}\text{sinc}\left[(b\alpha_k + d)\delta\sigma\right]\cos\Phi_k$

 $\Phi_k = 2\pi b \alpha_k \sigma + 2\pi d \sigma + \phi_s + \phi_o$

- • Modelling the interferograms: need to know the OPD
	- Iterative process (3 or 4 steps)
	- $1st$ step: assume OPD = 0 and model the interferograms
	- – $2nd$ step: 1st estimate the OPD from differential phase slope
	- –3rd step: inject estimated OPD and remodel the interferograms
	- – $4th$ step: if necessary repeat $2nd$ and $3rd$ steps

How to model the interferograms

- •Describing the 1st step \rightarrow $m_k = c_k R - d_k I = \frac{1}{2}(W_k C + W_k^* C^*)$
- \bullet $C = R + iI$ is the complex coherent energy of the object

$$
C=2V\sqrt{K_{1}K_{2}}\sqrt{\sum_{j=1}^{n}a_{1j}a_{2j}}\times e^{i\phi_{o}}e^{2i\pi d\sigma}
$$

• $W_k = c_k + id_k$ is the carrying wave of the interferometer

$$
W_k = \sqrt{\frac{a_{1k}a_{2k}}{\sum_{j=1}^n a_{1j}a_{2j}}} \times e^{i(2\pi f \alpha_k + \phi_s)}
$$

•The carrying wave is determined experimentally before the observations

The complex coherent energy

 \bullet C is estimated by minimizing \rightarrow

$$
\chi^2 = \sum_{k=1}^n \left(\frac{m_k - c_k R + d_k I}{\sigma_k} \right)^2
$$

 \bullet Which gives:

$$
R = \frac{\sum_{j=1}^{n} \frac{c_k m_k}{\sigma_k^2} \sum_{j=1}^{n} \frac{d_k^2}{\sigma_k^2} - \sum_{j=1}^{n} \frac{d_k m_k}{\sigma_k^2} \sum_{j=1}^{n} \frac{c_k d_k}{\sigma_k^2}}{\sum_{j=1}^{n} \frac{c_k^2}{\sigma_k^2} \sum_{j=1}^{n} \frac{d_k^2}{\sigma_k^2} - \left(\sum_{j=1}^{n} \frac{c_k d_k}{\sigma_k^2}\right)^2}
$$

$$
I = \frac{\sum_{j=1}^{n} \frac{c_k m_k}{\sigma_k^2} \sum_{j=1}^{n} \frac{c_k d_k}{\sigma_k^2} - \sum_{j=1}^{n} \frac{d_k m_k}{\sigma_k^2} \sum_{j=1}^{n} \frac{c_k^2}{\sigma_k^2}}{\sum_{j=1}^{n} \frac{c_k^2}{\sigma_k^2} \sum_{j=1}^{n} \frac{d_k^2}{\sigma_k^2} - \left(\sum_{j=1}^{n} \frac{c_k d_k}{\sigma_k^2}\right)^2}
$$

•

C is obtained by matrix transformation \rightarrow $\left[\begin{array}{c} R \\ \overline{F} \end{array}\right]$ m] x [P2VM]

 \bullet Generalisation to n telescopes immediate

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Estimates of the observables

• The visibility
$$
\rightarrow
$$
 $V^2 = \frac{|\mathcal{C}|^2 > -\langle b \rangle}{4 \langle \sum_{j=1}^n P_{1k} P_{2k} \rangle} = \frac{\langle R^2 \rangle + \langle I^2 \rangle - \langle b \rangle}{4 \langle \sum_{j=1}^n P_{1k} P_{2k} \rangle}$

- $C_1 C_2^* = Ge^{2i\pi d(\sigma_1 \sigma_2) + i(\phi_1 \phi_2) + \phi_s}$ The differential visibility \rightarrow •
- $\phi_1 \phi_2 = Arg \left\langle e^{-2i\pi d(\sigma_1 \sigma_2)} C_1 C_2^* \right\rangle \phi_s$ The differential phase \rightarrow •
- $\phi_{12} + \phi_{23} \phi_{13} = Arg \langle C_{12} C_{23} C_{13}^* \rangle \phi_s$ The closure phase \rightarrow •

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